STRUCTURAL DESIGN CALCULATIONS

COUNTY OF IMPERIAL CALIFORNIA

TABLE OF CONTENTS

- GRAVITY LOADS
- SECTION PROPERTIES
- ALLOWABLE STRESSES
- ALLOWABLE SHEAR
- SHEARWALL PANEL SCHEDULE
- TIMBER BEAM DESIGN
- SEISMIC FORCES/WIND FORCES
- FLOOR SHEARWALL DIAGRAM
- LATERAL LOADS
- ROOF DIAPHRAGM DESIGN
- SHEARWALL DESIGN
- CONTINUOUS FOOTING DESIGN

DESIGN CRITERIA AND SPECIFICATIONS

A. CODE: 2003 International Building Code ZONE FAULT TYPE Distance **B. SEISMIC:** Basic wind speed MPH.Exposure C. WIND: Allowable soil bearing pressure _____ psf D. SOILS: E. LUMBER: Douglas Fir-Larch, 1. 2X Joists & Rafters-#2 or Better 2. 4X, 6X, 8X Beams & Headers- #1 orBetter 3. Plates, Blocking & Studs – Stud Grade or Better F. GLUED-LAMINATED BEAM: Combination: 24 F- V4 Species: DF/DF PARALLAM BEAM: Truss Joist – MacMillan, 2.0E Parallam PSL MICROLLAM BEAM: Truss Joist - MacMillan, 1.9E Microllam LVL Non-Monolithic Pour Foundation System, U.N.O. G. CONCRETE: All slab-on-grade/ continuous footing/ pads / pole footing _____ f'c= 2500 psi All structural concrete/ retaining wall / column / beam / _____ f'c= 3000 psi ASTM A36, Fy = 36 ksi for Structural Steel H. STEEL: ASTM A615, Gr, 40 for #3 & 4, Gr.60 for # 5 and larger rebar steel ASTM A53, Gr. B for Pipe Steel ASTM A500, Gr. BB for Tube Steel I. CONCRETE BLOCK: ASTM C90, Grade N medium weight, Solid grouted all cells J. COLD FORM STEEL: ASTM A570-79 Gr.33 for 18 through 25 Gauge ASTM A570-79 Gr 50 for 12 through 16 Gauge K. WOOD CONSTRUCTION CONNECTOR: SIMPSON Strong-Tie or Approved Equal L. TRUSS CALCULATIONS: Provided by:

It is the full intention of the Engineer that these calculations conform to the International Building Code, 2003 edition. These calculations shall govern the structural portion of the working drawings. However, where any discrepancies occur between these calculations and the working drawings, the Engineer shall be notified immediately so proper action may be taken. The structural calculations included here are for the analysis and design of primary structural system. The attachment of non- structural elements is the responsibility of the architect or designer, unless specifically shown otherwise. The Engineer assumes no responsibility for work not a part of these calculations. When structural observation or field investigation the Engineer is required, the architect/ contractor shall make separate arrangements with the Engineer.

Project Name Job # \$5161

GRAVITY LOADS

ROOF

	Live Load	=	20 psf (for pitch 4:12 or greater)
	Dead Load		
	Roof cover	=	10 psf (for tile)
	1/2" Plywood Shuttering	=	1.5 psf
	Roof Framing	=	3.5 psf
	1/2" Drywall Ceiling	=	2.0 psf
	Insulation	=	2.0 psf
	D.L	=	19 psf
	Total Load	=	35 psf
EXTERNAL WALL			
	Dead Load		
	2x stud wall	=	1.5 psf
	1/2" Plywood Panel	=	1.5 psf
	1/2" Drywall	=	2.0 psf
	7/8" Stucco	=	10.0 ps
	Insulation	=	1.0 psf
	Total	=	16.0 psf
INTERNAL WALL			
	Dead Load		
	2x stud wall	=	1.5 psf
	3/8" Plywood Panel	=	1.1 psf
	(2)-1/2" Drywall	=	4.0 psf
	Misc	=	3.4 psf
	Total	=	10.0 psf
			-

NOMINAL	STANDARD DRESSED SIZE	AREA	MOMENT OF	SECTION MODULUS		in pounds of wood p				when
(inches)d	(S4S) b(inches)d	SECTION	INERTIA	S	25 lb.	30 1b.	35 1b.	40 1Ъ.	45 lb.	50 Ib
1×3	$3/4 \times 2 1/2$	1.875	0.977	0.781	0.326	0.391	0.456	0.521	0.586	0.65
1 x 4	$3/4 \times 3 1/2$	2.625	2.680	1.531	0.456	0.547	0.638	0.729	0.820	0.91
1 x 6	3/4 x 5 1/2	4.125	10.398	3.781	0.716	0.859	1.003	1.146	1.289	1.43
	3/4 x 7 1/4	5.438	23.817	6.570	0.944	1.133	1.322	1.510	1.699	1.88
1 x 8	3/4 x 9 1/4	6.938	49.466	10.695	1.204	1.445	1.686	1.927	2.168	2.40
1 x 10 1 x 12	3/4 x 11 1/4	8.438	88.989	15,820	1.465	1.758	2.051	2.344	2.637	2.93
2 x 3	1 1/2 x 2 1/2	3.750	1.953	1.563	0.651	0.781	0.911	1.042	1.172	1.30
2 x 4	$1 \frac{1}{2} \times 3 \frac{1}{2}$	5.250	5.359	3.063	0.911	1.094	1.276	1.458	1.641	1.82
2 x 6	1 1/2 x 5 1/2	8.250	20.797	7.563	1.432	1.719	2.005	2.292	2.578	2.86
2 × 8	1 1/2 x 7 1/4	10.875	47.635	13.141	1.888	2.266	2.643	3.021	3.398	3.77
2 x 10	1 1/2 x 9 1/4	13.875	98.932	21.391	2.409	2.891	3.372	3.854	4.336	4.81
2 x 12	1 1/2 x 11 1/4	16.875	177.979	31.641	2.930	3.516	4.102	4.688	5.273	5.85
2 × 14	1 1/2 x 13 1/4	19.875	290.775	43.891	3.451	4.141	4.831	5.521	6.211	6.90
3 x 1	2 1/2 x 3/4	1.875	0.088	0.234	0.326	0.391	0.456	0.521	0.586	0.65
3 x 2	2 1/2 x 1 1/2	3.750	0.703	0.938	0.651	0.781	0.911	1.042	1.172	1.30
3 x 4	2 1/2 x 3 1/2	8.750	8.932	5.104	1.519	1.823	2.127	2.431	2.734	3.03
3 x 6	2 1/2 x 5 1/2	13.750	34.661	12.604	2.387	2.865	3.342	3.819	4.297	4.77
3 x 8	2 1/2 x 7 1/4	18.125	79.391	21.901	3.147	3.776	4.405	5.035	5.664	6.29
3 x 10	2 1/2 x 9 1/4	23.125	164.886	35.651	4.015	4.818	5.621	6.424	7.227	8.03
3 x 12	2 1/2 x 11 1/4	28.125	296.631	52.734	4.883	5.859	6.836	7.813	8.789	9.76
3 x 14	2 1/2 x 13 1/4	33.125	484.625	73.151	5.751	6.901	8.051	9.201	10.352	11.50
3 × 16	2 1/2 x 15 1/4	38.125	738.870	96.901	6.619	7.943	9.266	10,590	11.914	13.23
4 x 1	3 1/2 x 3/4	2.625	0.123	0.328	0.456	0.547	0.638	0,729	0.820	0.91
4 x 2	3 1/2 x 1 1/2	5.250	0.984	1.313	0.911	1.094	1.276	1.458	1.641	1.82
4 x 3 *	3 1/2 x 2 1/2	8.750	4.557	3.646	1.519	1.823	2.127	2.431	2.734	3.03
4 x 4	3 1/2 x 3 1/2	12.250	12.505	7.146	2.127	2.552	2.977	3.403	3.828	4.25
4 x 6	3 1/2 x 5 1/2	19.250	48.526	17.646	3.342	4.010	4.679	5.347	6.016	6.68
4 x 8	3 1/2 x 7 1/4	25.375	111.148	30.661	4.405	5.286	6.168	7.049	7.930	8.81
4 x 10	3 1/2 x 9 1/4	32.375	230.840	49.911	5.621	6.745	7.869	8.933	10.117	11.24
4 x 12	3 1/2 x 11 1/4	39.375	415.283	73.828	6.836	8.203	9.570	10.938	12.305	13.67
4 x 14	3 1/2 x 13 1/4	46.38	678.5	102.4	8.051	9.661	11.27	12.88	14.49	16.10
4 x 16	3 1/2 × 15 1/4	53,38	1034	135.7	9.266	11.12	12.97	14.83	16.68	18.53
6 x 1	5 1/2 x 3/4	4.125	0.193	0.516	0.716	0.859	1.003	1.146	1.289	1.43
6 x 2	5 1/2 × 1 1/2	8.250	1,547	2.063	1.432	1.719	2.005	2.292	2.578	2.86
6 x 3	5 1/2 x 2 1/2	13.750	7.161	5.729	2.387	2.865	3.342	3.819	4.297	4.77
6 x 4	5 1/2 x 3 1/2	19.250	19.651	11.229	3.342	4.010	4.679	5.347	6.016	6.68
6 x 6	$5 1/2 \times 5 1/2$	30.250	76.255	27.729	5.252	6.302	7.352	8.403	9.453	10.50
6 x 8	5 1/2 x 7 1/2	41.250	193.359	51.563	7.161	8.594	10.026	11.458	12.891	14.32
6 x 10	5 1/2 x 9 1/2	52.250	392.963	82.729	9.071	10.885	12.700	14.514	16.328	18.14
6 x 12	$5 \frac{1}{2} \times \frac{11}{1} \frac{1}{2}$	63.250 74.250	697.068	121.229	10.981 12.891	13.177	15.373 18.047	17.569 20.625	19.766	21.96
6 x 14 6 x 16	5 1/2 × 13 1/2 5 1/2 × 15 1/2	85.250	1706.776	220.229	14.800	17.760	20.720		23.203	25.78
6 x 16 6 x 18	$5 \frac{1}{2} \times \frac{1}{17} \frac{1}{1/2}$	96.250	2456.380	280.729	16.710	20.052	23.394	23.681 26.736	30.078	29.60
6 x 20	5 1/2 x 19 1/2		3398.484	348.563	18.620	22.344	26.068	29.792	33.516	37.24
6 x 22	5 1/2 x 21 1/2		4555.086	423.729	20.530	24.635	28.741	32.847	36.953	41.05
6 x 24	5 1/2 x 23 1/2		5948.191	506.229	22.439	26.927	31.415	35.903	40.391	44.87
8 × 1	7 1/4 x 3/4	5.438	0.255	0.680	0.944	1.133	1,322	1.510	1.699	1.88
8 x 2	7 1/4 x 1 1/2	10.875	2.039	2.719	1.888	2.266	2.643	3,021	3.398	3.77
8 x 3	7 1/4 x 2 1/2		9.440	7.552	3.147	3.776	4.405	5.035	5.664	6.29
8 x 4	7 1/4 x 3 1/2		25.904	14.802	4.405	5.286	6.168	7.049	7.930	8.81
8 x 6	7 1/2 x 5 1/2		103.984	37.813	7.161	8.594	10.026	11.458	12.891	14.32
8 x 8	7 1/2 x 7 1/2		263.672	70.313	9.766	11.719	13.672	15.625	17.578	19.5
8 x 10	7 1/2 x 9 1/2		535.859	112.813		14.844	17.318	19.792	22.266	24.74
8 x 12	7 1/2 x 11 1/2		950.547	165.313	14.974	17.969	20.964	23.958	26.953	29.94
8 x 14	7 1/2 x 13 1/2		1537.734	227.813		21.094	24.609	28.125	31.641	35.15
8 x 16	7 1/2 x 15 1/2		2327.422	300.313	20.182	24.219	28.255	32.292	36.328	40.36
8 x 18	7 1/2 x 17 1/2		3349.609	382.813		27.344	31.901	36.458	41.016	45.5
8 × 20	7 1/2 x 19 1/2		4634.297	475.313		30.469	35.547	40.625	45.703	50.78
8 x 22 8 x 24	7 1/2 x 21 1/2 7 1/2 x 23 1/2		6211.484	577.813		33.594	39.193	44.792 48.958		55.99
V A 24		110.250	8111.172	690.313	30.599	36.719	42.839	40.750	55.078	61.1

NOMINAL	STANDARD DRESSED	AREA OF	MOMENT OF	SECTION	Weight weight	in pounds of wood p	per line er cubic	ar foot foot equ	of piece als:	wnen
SIZE	SIZE (S45)	SECTION	INERTIA	S	25 1b.	30 1ь.	35 1b.	40 1b.	45 1b.	50 1b.
(inches)d	b(inches)d				1,204	1.445	1.686	1.927	2.168	2.40
10 x 1	9 1/4 x 3/4	6.938	0.325	0.867 3.469	2.409	2.891	3.372	3.854	4.336	4.81
10 × 2	9 1/4 x 1 1/2	13.875	12.044	9.635	4.015	4.818	5.621	6,424	7.227	8.03
10 x 3 10 x 4	9 1/4 x 2 1/2 9 1/4 x 3 1/2	32.375	33.049	18.885	5.621	6.745	7.869	8.993	10.117	11.24
10 x 4 10 x 6	9 1/2 x 5 1/2	52.250	131.714	47.896	9.071	10.885	12.700	14.514	16.328	18.14
10 x 8	9 1/2 x 7 1/2	71.250	333.984	89.063	12.370	14.844	17.318	19.792	22.266	24.74
10 × 10	9 1/2 x 9 1/2	90.250	678.755	142.896	15.668	18.802	21.936	25.069 30.347	28.203	37.93
10 x 12	9 1/2 x 11 1/2	109.250	1204.026	209.396	18.967	22.760 26.719	26.554 31.172	35.625	40.078	44.53
10 x 14	9 1/2 x 13 1/2	128.250	1947.797 2948.068	288.563 380.396	25.564	30.677	35.790	40.903	46.016	51.12
10 x 16	9 1/2 x 15 1/2 9 1/2 x 17 1/2	147.250 166.250	4242.836	484.896	28,863	34.635	40.408	46.181	51.953	57.72
10 x 18	9 1/2 x 17 1/2 9 1/2 x 19 1/2	185.250	5870.109	602.063	32.161	38.594	45.026	51.458	57.891	64.32
10 x 20 10 x 22	9 1/2 x 21 1/2	204.250	7867.879	731.896	35.460	42.552	49.644	56.736	63.828	70.92
10 x 24	9 1/2 x 23 1/2	223.250	10274.148	874.396	38.759	46.510	54.262	62.014	69.766	77.51
12 x 1	11 1/4 x 3/4	8.438	0.396	1.055	1.465	1.758	2.051	2.344	2.637	2.93
12 x 2	11 1/4 x 1 1/2	16 875	3.164	4.219	2.930	3.516	4.102	4.688	5.273	5.85 9.76
12 × 3	11 1/4 x 2 1/2	28.125	14.648	11.719	4.883	5.859 8.203	6.836 9.570	10 938	12.305	13.67
12 × 4	11 1/4 x 3 1/2	39.375	40.195	22.969	6.836	13.177	15.373	17.569	19.766	21.96
12 × 6	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	63.250 86.250	404.297	107.813	14.974	17.969	20.964	23.958	26,953	29.94
12 x 8 12 x 10	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	109.250	821.651	172.979	18.967	22.760	26.554	30.347	34.141	37.93
12×10 12 x 12	11 1/2 x 11 1/2	132.250	1457.505	253.479	22.960	27.552	32.144	36.736	41.328	45.92
12 x 14	11 1/2 x 13 1/2	155.250		349.313	26.953	32.344	37.734	43.125 49.514	48.516	53.90
12 x 16	11 1/2 x 15 1/2	178.250		460.479	30.946	37.135	43.325	55.903		69.87
12 x 18	11 1/2 x 17 1/2	201.250		586.979	38.932	46.719	54.505	62.292	70.078	77.86
12 × 20	11 1/2 x 19 1/2 11 1/2 x 21 1/2	224.250 247.250		885.979	42.925	51.510	60.095	68.681	77.266	85.85
12 x 22 12 x 24	11 1/2 x 23 1/2		12437.129	1058.479	46.918	56.302	65.686	75.069	84.453	93,8:
14 x 2	13 1/4 x 1 1/2	19.875	3.727	4.969	3.451	4.141	4.831	5.521	6.211	6.90
14 x 3	13 1/4 x 2 1/2	33.125	17.253	13.802	5.751	6.901	8.051	9.201	10.352	11.50
14 x 4	13 1/2 x 3 1/2	47.250		27.563	8.203	9.844	11.484	13.125	14.766 23,203	16.40
14 x 6	13 1/2 x 5 1/2	74.250		68.063	12.891	15.469	24.609	28.125		35.1
14 x 8	$13 1/2 \times 7 1/2$	101.250		203.063		26.719	31.172	35,625	40.078	44.5
14 x 10 14 x 12	13 1/2 x 9 1/2 13 1/2 x 11 1/2	155.250		297.563		32.344	37.734	43.125	48.516	53.90
14 x 16	13 1/2 x 15 1/2	209.250		540.563	36.328	43.594	50.859	58.125		72.6
14 x 18	13 1/2 x 17 1/2	236.250		689.063		49.219	57.422	65.625		82.0
14 x 20	13 1/2 x 19 1/2			855.563		54.844 60.469	63.984	80.625		100.7
14 x 22 14 x 24	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		11180.672	1040.063	Contraction of the second second	66.094	77.109	88.125		110.1
	15 1/2 x 2 1/2			16.146		8.073	9.418	10.764	12.109	13.4
16 x 3 16 x 4	15 1/2 x 3 1/2			31.646		11.302	13,186	15.069		18.8
16 x 6	15 1/2 x 5 1/2			78.146		17.760	20.720	23.681		29.6
16 x 8	15 1/2 x 7 1/2			145.313		24.219	28.255	32.292		40.3
16 x 10	15 1/2 x 9 1/2			233.146		30.677	43,325	49.514		61.8
16 x 12	15 1/2 x 11 1/2 15 1/2 x 13 1/2			470.813		43.594	50.859	58,125		72.6
16 x 14 16 x 16	15 1/2 x 15 1/2			620.646		50.052	58.394	66.736		83,4
16 x 18	15 1/2 x 17 1/2			791.146			65.929	75.347	84.766	
16 x 20	15 1/2 x 19 1/2			982.313		62.969	73.464 80.998		94.453	
16 × 22	$15 1/2 \times 21 1/2$		12837.066				88.533		113.828	
16 x 24	15 1/2 x 23 1/2	+	16763.086				23.394	26.736	1	
18 x 6 18 x 8	17 1/2 x 5 1/2 17 1/2 x 7 1/2						31.901	36.458	41.016	45.5
18 x 10	$17 1/2 \times 9 1/2$ 17 1/2 × 9 1/2				28.863	34.635	40.408	46.181		
18 × 12	17 1/2 x 11 1/2		2217.943	385,729			48.915	55,903		
18×14	17 1/2 × 13 1/2						57.422	65.625		
18 x 16	17 1/2 x 15 1/2						74.436	85.069		106.3
18 x 18 18 x 20	17 1/2 x 17 1/2 17 1/2 x 19 1/2		10813.359				82.943	94.793	106.641	118.4
18 x 20	17 1/2 x 21 1/2	376.250	14493.461	1348.229	65.321	78.385	91.450		117.578	
18 x 24	17 1/2 x 23 1/2	411.250	18926.066	1610.729	71.398	85.677	99.957	114.236	128.516	142.7

Allowable offess for visually Graded Lumber from 97 NDS

Douglas Fir-Larch

Grading Rule Agency: WCLIB/WWPA

	Size	Selec	t Strue	cture	No.1 8	& bette	er	No.	1		No	2		No.2	Repe	titive
Size	Factor	Fb	Fv	E	Fb	F٧	E	Fb	Fv	E	Fb	Fv	E	Fb	Fv	E
0120	CF	1450	95	1.9	1150	95	1.8	1000	95	1.7	875	95	1.6	875	95	1.6
2X4	1.5	2175	95	1.9	1725	95	1.8	1500	95	1.7	1350	95	1.6	1552	95	1.6
2X6	1.3	2885	95	1.9	1495	95	1.8	1300	95	1.7	1170	95	1.6	1345	95	1.6
2X8	1.2	1740	95	1.9	1380	95	1.8	1200	95	1.7	1080	95	1.6	1242	95	1.0
2X10	1.1	1595	95	1.9	1265	95	1.8	1100	95	1.7	990	95	1.6	1138	95	1.0
2X12	1)	1450	95	1.9	1150	95	1.8	1000	95	1.7	900	95	1.6	1035	95 95	1.0
2X14	0.9	1305	95	1.9	1035	95	1.8	900	95	1.7	810	95	1.6	931	95	1.0
4X4	1.5	2175	95	1.9	1725	95	1.8	1500	95	1.7	1313	95	1.0	1510	05	
4X6	1.4	1885	95	1.9	1495	95	1.8	1300	95	1.7	1138	95	1.6 1.6	1510	95	1.6
4X8	1.3	1885	95	1.9	1495	95	1.8	1300	95	1.7	1138	95	1.6	1309	95 95	1.0
4X10	1.2	1740	95	1.9	1380	95	1.8	1200	95	1.7	1050	95	1.6	1207	95 95	1.6
4X12	1.1	1595	95	1.9	1265	95	1.8	1100	95	1.7	963	95	1.6	1107	95	1.0
4x14 & UP	1)	1450	95	1.9	1150	95	1.8	1000	95	1.7	875	95	1.6	1006	95 95	1.0

-CR HEM-FIR: 975 75 1.5

FOR HEM FIR : 850 75 1.3 Fc = 405

Allowable Stress for Visually Graded Lumber from 97 NDS

D				
loug	00	- 1 P	aroh	
Doug	15	- II -	arch	
Dudy	100	1 11	Laion	

Grading Rule Agency: WCLIB/WWPA

LISE

		Size Factor	Select	Struc	lure	Den	se No	o. 1	No.	1		٨	lo. 2	
Size	d	1/9	Fb	Fv	Е	Fb	Fv	E	Fb	Fv	E	Fb	Fv	E
		CF = (12/d)	1600	85	1.6	1550	85	1.7	1350	85	1.6	875	85	1
6X6	5.5	1.0	1600	85	1.6	1550	85	1.7	(1350	85	1.6	875	85	1.
6X8	7.5	1.0	1600	85	1.6	1550	85	1.7	7350	85	1.6	875	85	1.
6X10	9.5	1.0	1600	85	1.6	1550	85	1.7	1350	85	1.6	875	85	1.
6X12	11.5	1.0	1600	85	1.6	1550	85	1.7	1350	85	1.6	875	85	1.
6X14	13.5	0.99	1579	85	1.6	1530	85	1.7	1332	85	1.6	864	85	1.
6X16	15.5	0.97	1555	85	1.6	1507	85	1.7	1312	85	1.6	850	85	1.
6X18	17.5	0.96	1534	85	1.6	1486	85	1.7	1295	85	1.6	839	85	1.
6X20	19.5	0.95	1516	85	1.6	1469	85	1.7	1279	85	1.6	829	85	1.
											_			

Note: Duration of Load. NDS TABLE 2.3.2

The allowable stress may increase as follows:

15% for snow load

USE $1050 \ 70 \ 1.3$ $F_{c} = 405^{-1}$

FOR HEMFIR:

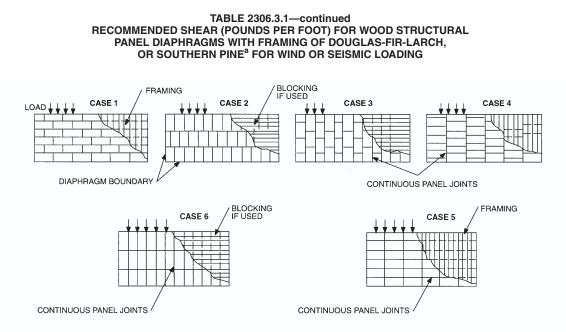
25% for seven days duration as for roof loads

Fb for 2x and 4x member have been multiplied by the repetitive member factor of 1.15 when such members are used as joist, truss chords, rafters, studs, planks, decking, or similar members which are spaced not more than 24 inches on center.

				BLOCKED DIAPHRAGMS UN		BLOCKED D	BLOCKED DIAPHRAGMS		UNBLOCKED DIAPHRAGMS	HRAGMS
				1	Fastener spa cases) at (Cases 3, 4	Fastener spacing (inches) at diaphragm boundaries (all cases) at continuous panel edges parallel to load (Cases 3, 4), and at all panel edges (Cases 5 and 6) ^b	t diaphragm bc nel edges paral nel edges (Case	oundaries (all llel to load is 5 and 6) ^b	Fasteners spaced 6" max. At supported edges ^b	," max. At Jes ^b
					6	4	2 ¹ / ₂ °	2°		
	ONINON NAIL SIZE OR STAPLE ¹			NOMINAL WIDTH OF FRAMING	Fastene	Fastener spacing (inches) at other panel edges (Cases 1, 2, 3 and 4) ^b	es) at other par 2, 3 and 4) ^b	lel edges	Case 1	All other
PANEL GRADE	LENGTH AND GAGE	IN FRAMING (inches)	THICKNESS (inch)	MEMBER (inches)	6	9	4	3	(No unblocked edges or continuous joints parallel to load)	configurations (Cases 2, 3, 4, 5 and 6)
	10	11		2	185	250	375	420	165	125
	bďč	1 1 4	15	3	210	280	420	475	185	140
	$1^{1/2}$		7/16	2	155	205	310	350	135	105
	16 Gage	_		3	175	230	345	390	155	115
	Ċ	13/		2	270	360	530	600	240	180
Structural I	80	17/8	3,	3	300	400	600	675	265	200
Grades	$1^{1/2}$		8/_	2	175	235	350	400	155	115
	16 Gage	_		3	200	265	395	450	175	130
	p1 0 1	11/		2	320	425	640	730	285	215
	1002	17/2	157	3	360	480	720	820	320	240
	$1^{-1}/_{2}$		132	2	175	235	350	400	155	120
	16 Gage	_		3	200	265	395	450	175	130
	61 V	1		2	170	225	335	380	150	110
	00,	1-74	51	3	190	250	380	430	170	125
Sheathing, single floor	$1^{-1}/_{2}$,16	2	140	185	275	315	125	06
and other	16 Gage	-		3	155	205	310	350	140	105
grades covered in	9E 2	11/		2	185	250	375	420	165	125
DOC PS 1 and PS 2	200	1 /4	3,	3	210	280	420	475	185	140
	FO	13/		2	240	320	480	545	215	160
	ρο	r /8		3	270	360	540	610	240	180

(continued)

TABLE 2306.3.1 RECOMMENDED SHEAR (POUNDS PER FOOT) FOR WOOD STRUCTURAL PANEL DIAPHRAGMS WITH FRAMING OF DOUGLAS-FIR-LARCH, OR SOUTHERN PINE^a FOR WIND OR SEISMIC LOADING



For SI: 1 inch = 25.4 mm, 1 pound per foot = 14.5939 N/m.

- a. For framing of other species: (1) Find specific gravity for species of lumber in AFPA National Design Specification. (2) For staples find shear value from table above for Structural I panels (regardless of actual grade) and multiply value by 0.82 for species with specific gravity of 0.42 or greater, or 0.65 for all other species. (3) For nails find shear value from table above for nail size for actual grade and multiply value by the following adjustment factor: Specific Gravity Adjustment Factor = [1-(0.5 SG)], where SG = Specific Gravity of the framing lumber. This adjustment factor shall not be greater than 1.
- b. Space fasteners maximum 12 inches o.c. along intermediate framing members (6 inches o.c. where supports are spaced 48 inches o.c.).
- c. Framing at adjoining panel edges shall be 3 inches nominal or wider, and nails shall be staggered where nails are spaced 2 inches o.c. or 2¹/₂ inches o.c.
- d. Framing at adjoining panel edges shall be 3 inches nominal or wider, and nails shall be staggered where both of the following conditions are met: (1) 10d nails having penetration into framing of more than $1^{1}/_{2}$ inches and (2) nails are spaced 3 inches o.c. or less.
- e. 8d is recommended minimum for roofs due to negative pressures of high winds.
- f. Staples shall have a minimum crown width of $^{7}/_{16}$ inch.

SHEAR WALL PANEL SCHEDULE

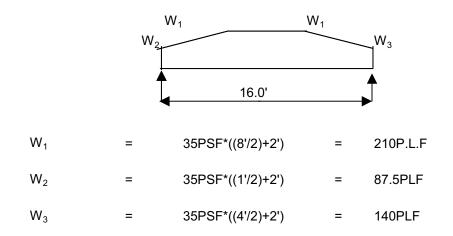
			Γ	
MARK	WALL TYPE & NAIL SPACING (COMMON OR BOX)	ALLOWABLE SHEAR,PLF	ANCHOR BOLTS (12" LONG OR 15" FOR 2- POUR)	UPPER FLOOR SILL NAILING
	5/8" Drywall, blocked, with 6d cooler nails @ o.c at edges and field.	85.5 (*175)	5/8" @ 6'(*5/8 @ 3') DBL SIDED	16d @ 16" (*16d @ 8")
8	7/8" stucco over paper backed lath w/11 Ga.x1.5" galv. Nail @ 6" o.c at top and bottom plates, edge of wall and in field .see note # 3 below.	180	5/8" @ 6'	16d @ 8"
10	3/8" CDX plywood or OSB w/8d nails @ 6" o.c at edges and @ 12" o.c in field. See note # 5 below.	260 (*520)	5/8"@ 4' (*5/8" @ 2')IF DBL SIDED	16D @ 6" (*16d @ 3")
	3/8" CDX plywood or OSB w/8d nails @ 4" o.c at edges and @ 12" o.c in field .USE 3X FOUNDATION SILL PLATE & 3X STUDS AND BLOCKS AT ADJACENT PANELS.	380 (*760)	5/8"@ 4' (*5/8" @ 2')IF DBL SIDED	16D @ 4" (*16d @ 2")
	3/8" CDX plywood or OSB w/8d nails @ 3" o.c at edges and @ 12" o.c in field .USE 3X FOUNDATION SILL PLATE & 3X STUDS AND BLOCKS AT ADJACENT PANELS.	490 (*980)	5/8"@ 3' (*5/8"@ 1.5')IF DBL SIDED	16D @ 3.5" (*2-16d @ 3.5")
13	3/8" CDX plywood or OSB w/8d nails @ 2" o.c at edges and @ 12" o.c in field .USE 3X FOUNDATION SILL PLATE & 3X STUDS AND BLOCKS AT ADJACENT PANELS.	640 (*1280)	5/8"@ 18" (*5/8" @ 14")IF DBL SIDED	16D @2.5" (*2-16d @ 2.5")
	¹ / ₂ " Str. 1 plywood w/10d nails @ 2" o.c of edges and @ 12" o.c in field. USE 3X FOUNDATION SILL PLATE & 3X STUDS AND BLOCKS AT ADJACENT PANELS.	870 (*1740)	5/8"@ 20" (*5/8" @ 10")IF DBL SIDED	16D @2" (*2-16d @ 2")

NOTES:

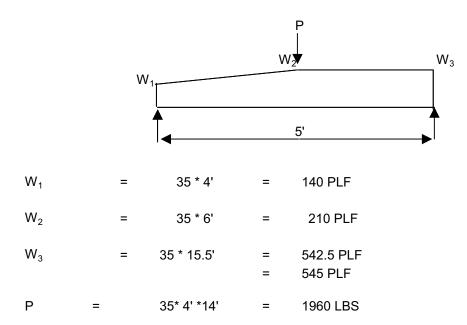
- (*----) in the table designates that shear wall sheating is to be applied on both faces of wall.
 All plywood edges must be blocked with 2x solid blocking. Field nailing shall be 12" o.c for stud spaced at 16" o.c and 6" o.c otherwise.
 Paper hacked self-furring expanded metal lath with ICBO approval.
- 4. Where allowable shear values exceed 350 plf, foundation sill plates and all framing members receiving
- 5. All interior bearing and non- bearing footing's shall have 7/32" shot pins @ 32" o.c & 48" o.c respectively.
- 6. All anchor bolt shall have plate wahers a minimum of 2"x2"x3/16" thick.

LOAD CALCULATIONS

BM#1-16' GARAGE DR.HDR



BM#2-HDR AT REAR OF MASTER BEDROOM



General Timber Beam

Description BM#1-16' GARAGE DR.HDR

Section Name 4x14		Co	nter Sp	20	16.0	0 ft	Lu	0.0)0 ft
Beam Width	3.500 in		ft Canti		10.0		Lu		0 ft
Beam Depth	13.250 in		ght Can			ft	Lu	0.0	00 ft
Member Type	Sawn			ir - Larch, N					
Bm Wt. Added to Loads Load Dur. Factor	1.250		Base A	Allow	1,000	•			
Beam End Fixity	Pin-Pin		Allow			0 psi 0 psi			
Wood Density	35.000 pcf	E	/		1,700				
pezoidal Loads									
#1 DL @ Left	87.50 #/ft	LL @ Le			#/ft	Start		0.000	
DL @ Right	210.00 #/ft	LL @ Rig			#/ft	End		6.500	
#2 DL @ Left DL @ Right	210.00 #/ft 210.00 #/ft	LL @ Le LL @ Rig			#/ft #/ft	Start End		6.500 12.000	
#3 DL @ Left	210.00 #/ft	LL @ Ki			#/ft	Start		12.000	
DL @ Right	210.00 #/ft	LL @ Le			#/ft	End		12.000	
	140.00 #/11		JIIL		#/IL	LIIU	LUC	10.000	it.
Summary								Bea	m Design Ok
Span= 16.00ft, Beam W	idth = 3.500in x De	epth = 13.25	5in. End	ls are Pin-Pi	n				
Max Stress Ratio	(0.615 : 1	,						
Maximum Moment		6.6 k-ft		Ма	aximum	Shear *	1.5		2.1 k
Allowable		10.7 k-ft			Allowa	ble			5.5 k
Max. Positive Moment Max. Negative Moment	6.56 k-ft -0.00 k-ft		8.192 16.000		SI	near:	@ Left @ Right		1.41 k 1.59 k
Max @ Left Support	0.00 k-ft				C	amber:	@ Left		0.000 in
Max @ Right Support	0.00 k-ft						@ Cente	r	0.389 in
Max. M allow	10.67			Reactions			@ Right		0.000 in
fb 768.67 psi	fv	45.70 psi		Left DL	1.41	k	Max		1.41 k
Fb 1,250.00 psi	Fv	118.75 psi		Right DL	1.59)k	Max		1.59 k
ections									
Center Span	Dead Load	Total L			antilever		Dead Load		Total Load
Deflection	-0.259 in		259 in		flection	£1	0.000		0.000 in
Location Length/Defl	8.064 ft 740.7	8.0 740)64 ft 71		Length/De		0.0)	0.0
Camber (using 1.5 * D.L		740		•	Cantilever flection		0.000	lin	0.000 in
@ Center	0.389 in				Length/De	fl	0.000		0.000 III
@ Left	0.000 in				0		0.0		0.0
@ Right	0.000 in								

General Timber Beam

Description

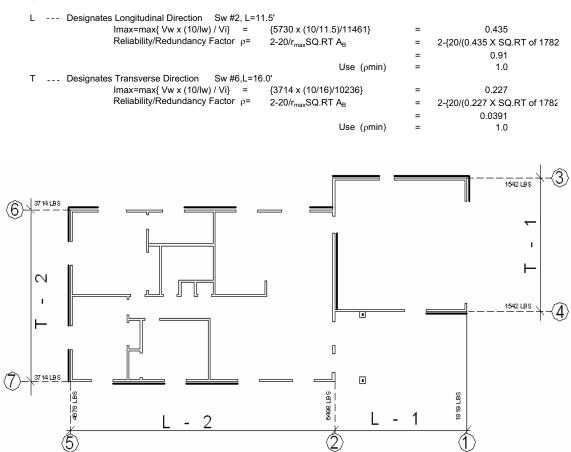
DN BM#2- HDR AT REAR OF MASTER BEDROOM

General Information		Calculation	ns are des	igned to	1997 ND	S and 19	97 UBC	Requirements
Section Name 4x12 Beam Width Beam Depth Member Type Bm Wt. Added to Loads Load Dur. Factor Beam End Fixity Wood Density	3.500 in 11.250 in Sawn 1.250 Pin-Pin 35.000 pcf	Right C Dougla	ntilever Cantilever Is Fir - Larch, Ise Allow W	No.1 1,000 95	.0 psi .0 psi	.Lu	0.00 fr 0.00 fr 0.00 fr	
Trapezoidal Loads								
#1 DL @ Left DL @ Right #2 DL @ Left DL @ Right	140.00 #/ft 210.00 #/ft 545.00 #/ft 545.00 #/ft	LL @ Left LL @ Right LL @ Left LL @ Right		#/ft #/ft #/ft #/ft	Start L End Lo Start L End Lo	0C 0C	0.000 ft 3.500 ft 3.500 ft 5.000 ft	
Point Loads								
Dead Load 1,960.0 lbs Live Load lbs distance 3.500 ft			bs bs t 0.0	lbs Ibs 000 ft		os os	lbs Ibs).000 ft	-0.3 lbs lbs 0.000 ft
Span= 5.00ft, Beam Wid Max Stress Ratio	•	th = 11.25in, Ei 0.580 <u>:</u> 1	nds are Pin-Pi	n			Beam	Design OK
Maximum Moment Allowable		2.9 k-ft 8.5 k-ft	N	laximum Allowa		1.5	2.7 4.7	
Max. Positive Moment Max. Negative Moment Max @ Left Support Max @ Right Support Max. M allow	2.86 k-ft -0.00 k-ft 0.00 k-ft 0.00 k-ft 8.46		500 ft 000 ft Reactions.	С	hear: amber:	 @ Left @ Right @ Left @ Center @ Right 	r	1.12 k 2.32 k 0.000 in 0.023 in 0.000 in
fb 464.10 psi Fb 1,375.00 psi	fv Fv	68.92 psi 118.75 psi	Left DL Right DL	1.12 2.32		Max Max		1.12 k 2.32 k
Deflections								
Center Span Deflection Location Length/Defl Camber (using 1.5 * D.L. @ Center @ Left @ Right	<u>Dead Load</u> -0.015 in 2.700 ft 3,921.8 Defl) 0.023 in 0.000 in 0.000 in	<u>Total Load</u> -0.015 2.700 3,921.77	n C ft Righ t	Cantilever Deflection Length/De Cantilever Deflection Length/De	fl 	Dead Load 0.000 0.0 0.000 0.0	in	otal Load 0.000 in 0.0 0.000 in 0.0

SEISMIC FORCES

Seismic zone 4 Soil profile Bearing wall system Seismic fault:	4 =	Z S _D	=	0.4		
Bearing wall system	=	S _D				
Seismic fault:		R	=	5.5		
Closest distance to the fau	lt		=	1.35		
Seismic coefficient		C _a	=	0.44		
Standard occupancy		N _a I	=	0.594 1		
Simplified total design ba	ase shear:					
		V		(3.0C _a /R) 0.324		W W
Forces at each level:		Fx	=	(3.0Ca/R)		wi
Diaphragm force:				(*******)		
		Fpx	=	(3.0Ca/R)		wpx
For allowable stress desi	ign					
		V _{ASD}		V/1.4 0.23143		W
WIND FORCES						
Design Wind Pressure						
		Р	=	$C_e \; C_q \; q_s \; I_w$		(20-1)
Combined Height, Exposu	re and Gues					(Table16-G)
		Ce	=	1.06		
		Ce Ce	=			
		Ce	=	1.19 1.23		
		Ce	=	1.31		
		н		0-15'.Expo		
		H H		20'. Expo 25'. Expo		
		Н		30'. Expo		
		н		40'. Expo		
Pressure Coefficient						(Table 16-II)
		Cq	=	1.3		Primary frame, projected area method
		Cq	=	1.2		Wall not in discontinuity area
		Cq Cq	=	1.5 1.6		all corners in discontinuity area(outward win Partially enclosed structure wall
Wind Stagnation Pressure	e at Standa	rd Height of 33 fe	et			(Table 16-F)
		q _s	=	12.6	psf	Basic Wind Speed=70MPH
		q _s	=	16.4	psf	Basic Wind Speed=80MPH
		q _s	=	20.8	psf	Basic Wind Speed=90MPH
Standard Occupancy		l _w	=	1		(Table 16-K)
Standard Occupancy Mean Roof Height		l _w	=	11.0625	feet	(Table 16-K)
		l _w P			feet feet psf	(Table 16-K)

___1st___ FLOOR SHEAR WALL DIAGRAM



O --- Designates Shear Wall Number

(

LATERAL LOADS

Section	Reliability/ Redu <u>L-1</u> <u>Input:</u>	Indancy Factor Seismic Coefficie Wind Pressure Roof weight Floor weight Exterior wall weig Interior wall weig Roof height	ght		1.00 0.231 22.6psf 19.0 0.0 16.0 10.0				
		Roof depth		=	25.0				
		Wall height		=	8.0				
		Floor depth # of exterior walls	2	=	0.0 LATERAL LOADS				
		# of interior walls		=	0.0				
	Wind Load,		Vw	=	22.6*(3.0+8.0/2)	=	158.2 plf	∢	controls
	Seismic Load,	Roof DL		=	19.0*25.0	=	475.0		
	Seisinic Load,	Floor DL		_		=			
		Ext.Wall DL		=		=	128.0		
		Int.Wall DL		=		=	0.0		
				=	475 0 0 0 100 0 0 0	_	602 0alf		
		Total DL,W Seismic Load		=		=	603.0plf 139.3plf		
		0000000 20000							
Section	<u>L-2</u>								
	<u>Input:</u>	Roof height		=	5.0				
		Roof depth		=	31.0				
		Wall height		=	8.0				
		Floor depth	_	=	0.0				
		# of exterior walls # of interior walls		=	2.0 1.5				
				-	1.5				
	Wind Load,		Vw	=	22.6*(5.0+8.0/2)	=	203.4plf	∢	controls
	Seismic Load,	Roof DL		=	19.0*31.0	=	589.0		
		Floor DL		=	0.0*0.0	=	0.0		
		Ext.Wall DL		=	2*16.0*8.0/2	=	128.0		
		Int.Wall DL		=	2*10.0*8.0/2	=	60.0		
		Total DL,W		=	589.0+0.0+128.0+60.0	=	777.0plf		
		Seismic Load		=	0.231*777.0*1.00	=	179.5plf		

LATERAL LOADS

	Reliability/ Redu	ndancy Factor Seismic Coefficier Wind Pressure Roof weight Floor weight Exterior wall weigh Interior wall weigh	nt = = = ht =	=	1.00 0.231 22.6 19.0 0.0 16.0 10.0				
Section	<u>T-1</u>								
	Input:	Roof height Roof depth Wall height Floor depth # of exterior walls	=	=	2.5 25.0 8.0 0.0 1.0				
		# of interior walls		=	1.0				
	Wind Load,		Vw =	=	22.6*(2.5+8.0/2)	=	146.9plf	∢	controls
	Seismic Load,	Roof DL Floor DL Ext.Wall DL Int.Wall DL Total DL,W Seismic Load	= = =	=	19.0*25.0 0.0*0.0 1*16.0*8.0/2 1*10.0*8.0/2 475.0+0.0+64.0+40.0 0.231*579.0*1.00	= = = =	475.0 0.0 64.0 40.0 579.0plf 133.7plf		
Castian									
Section	<u>L-2</u> Input:	Roof height Roof depth Wall height Floor depth # of exterior walls # of interior walls	:	=	3.0 53.0 8.0 0.0 1.0 3.0				
	Wind Load,		Vw =	=	22.6*(3.0+8.0/2)	=	158.2plf		
	Seismic Load,	Roof DL Floor DL Ext.Wall DL Int.Wall DL	=	=	19.0*53.0 0.0*0.0 1*16.0*8.0/2 3*10.0*8.0/2	= = =	1007.0 0.0 64.0 120.0		
		Total DL,W Seismic Load		=	1007.0+0.0+64.0+120.0 0.231*1191.0*1.00	=	1191.0plf 275.1plf	∢	controls

ROOF DIAPHRAGM DESIGN

ROOF DIAPHRAGM

Direction:	L-2	Between Shear Wa Width L(ft) Depth D(ft)		2&5 = 46 27			
Diaphragm Force:		Wind Load Seismic Load Fpx	= =	179.5plf (3.0Ca/R)Wpx	Cntl 203.4 plf 		
Diaphragm Shear	=	203.4x(L/2)D	=	173.3 plf			
Use: 1/2" APA Rated Sheathing, or O.S.B. unblocked disphragm, exterior grade, Index 24/0 w/8 nails@6"o.c. at edges and boundaries, @12" o.c in field							
Splice Chord Force,	F=	M/D= 1/8 x 203.4 x	x (46.0)**2/2	7.0=1993lb			
16d sinker nails: allowable shear for double top plate, single shear, 1.5" penetration(p) v = 103lbs x Cd = 103 x (p/12 dia.) = 103 x (1.5"/12x0.135") = 95lbs Top Plate Splice: n = $F/(1.33x95)$							
	=	1993/127 15.7					
Use(16)- 16d sinkers							

SHEAR WALL LINE # 1

PANEL DESIGN:										
Section a-	Tributary width(ft)	=	23.0	S	eismic(plf)	=	139.3	Wind(plf)	=	158.2
Section b-	Tributary width(ft)	=	0.0	S	Seismic(plf)	=	0	Wind(plf)	=	0
Seismic load at Total seismic load =	oove this floor(lb) 139.3*23/2+0	=	0 1602lbs			Wind load	above this	floor(lb)	=	0
Total wind load =	158.2*23/2+0	_	1819lbs	← c	ontrols					
Total panel length =	3'-8"									
Shear =	1819/3.67	=	495.6lb/ft							
>>> Panel type used	3/8" CDX Plywood, Mark-	13	see sheet S	D1 for naili	na shadula					
and type used	5/6 ODX Tywood, Mark-	\sum	300 31001 0		ng sneuuie					
OVERTURNING ANALYSIS:										
Panel length(ft) =	<u>Panel # 1</u> 3.67	Panel # 2 0.00		Panel # 4 F 0.00	<u>anel # 5</u> 0.00	Panel # 6 0.00				
Panel height(ft) =	3.07	0.00		0.00	0.00					
Uplift due to lateral load(lb) =	3639	0		0	0					
Dead load on the panel (lb) =		0		0	0					
Roof tributary(fl Floor tributary(f	· · · · · · · · · · · · · · · · · · ·	0.0 0.0		0.0 0.0	0.0 0.0					
Wall weight(psf	·/	0.0		0.0	0.0					
Uplift of this floor(lb) =	, 391	0		0	0					
Uplift from upper floor(lb) =	0	0		0	0					
Total hold-down force(lb)= >>> Hold-down Typ e	3391 STHD14	0	0	0	0	0				
real noid-down rypc	0111014									
		SHEAR V	VALL LINE #	<u># 2</u>						
PANEL DESIGN: Section a-	Tributary width(ft)	=	23.0	c	Seismic(plf)	=	139.3	Wind(plf)	=	158.2
Section b-	Tributary width(ft)	=	23.0 46.0		Seismic(plf)	=	179.5	Wind(plf)	=	203.4
	pove this floor(lb)	=	0	-		Wind load	above this	,	=	0
Total seismic load =	139.3*23/2+179.5*46/2+0	=	5730lbs							
Total wind load = Total panel length =	158.2*23/2+203.4*46/2+0	=	6498lbs	← c	ontrols					
Total panel length = Shear =	11.5 ft 6498/11.5	=	565.0lb/ft							
		\wedge								
>>> Panel type used	3/8" CDX Plywood, Mark-		see sheet S	SD1 for naili	ng shedule					
OVERTURNING ANALYSIS:										
		Panel # 2	Panel # 3	Panel # 4 F	anel # <u>5</u>	Panel # 6				
Panel length(ft) =	11.5	0.00		0.0	0.0					
Panel height(ft) = Uplift due to lateral load(lb) =	8 4520	0.0 0		0	0 0					
Dead load on the panel (lb) =		0		0	0					
Roof tributary(fl		0.0	0.0	0.0	0.0	0.0				
Floor tributary(f		0.0		0.0	0.0					
Wall weight(psf Uplift of this floor(lb) =) 10 4212	0		0	0					
Uplift from upper floor(lb) =	-212	0		0	0					
Total hold-down force(lb)=	4212	0	0	0	0	0				
>>> Hold-down Type	STHD14									
		SHEAR V	VALL LINE #	# 3						
		-								
PANEL DESIGN: Section a-	Tributany width/ft)	=	21.0	~	oiemio/alf)	=	133.7	Wind(nff)	=	146.9
Section b-	Tributary width(ft) Tributary width(ft)	_	0.0		Seismic(plf) Seismic(plf)	=	0	Wind(plf) Wind(plf)	=	146.9
	pove this floor(lb)	=	0.0	C	(11)		above this		=	0
Total seismic load =	133.7*21/2+0	=	1404lbs							
Total wind load = Total panel length =	146.9.2*21/2+0 8.0 ft	=	1542lbs	← c	ontrols					
Shear =	1542/8.0	=	192.8lb/ft							
		\wedge								
>>> Panel type used	3/8" CDX Plywood, Mark-	10	see sheet S	SD1 for naili	ng shedule					
OVERTURNING ANALYSIS:										
	<u>Panel # 1</u>		Panel # 3			Panel # 6				
Panel length(ft) =	4.00	4.0		0.0	0.0					
Panel height(ft) = Uplift due to lateral load(lb) =	8.0 1542	8.0 1542		0 0	0 0					
Dead load on the panel (lb) =		248.0		0	0					
Roof tributary(fl) 3.0	3.0	0.0	0.0	0.0	0.0				
Floor tributary(f		0.0		0.0	0.0					
Wall weight(psf Uplift of this floor(lb) =) 16 1295	16 1295		0 0	0 0					
Uplift from upper floor(lb) =	0	1293		0	0					
Total hold-down force(lb)=	1295	1295	0	0	0					
>>> Hold-down Type	STHD14									

		SHEAR V	VALL LINE	# 4						
PANEL DESIGN:										
Section a-	Tributary width(ft)	=	21.0		Seismic(plf)	=		Wind(plf)	=	146.9
Section b-	Tributary width(ft)	=	0.0		Seismic(plf)	=		Wind(plf)	=	0
	ove this floor(lb)	=	0			Wind load	above this f	loor(lb)	=	0
Total seismic load = Total wind load =	133.7*21/2+0 146.9.2*21/2+0	=	1404 lbs 1542 lbs		controlo					
Total wind load = Total panel length =	7 ft	-	1042 105	•	controls					
Shear =	1542/7.0	=	220.4 lb/ft							
eneal	10121110	\wedge	2201110/10							
>>> Panel type used	3/8" CDX Plywood, Mark-	/10 \	see sheet	SD1 for na	iling shedule					
OVERTURNING ANALYSIS:										
			Panel # 3		Panel # 5	Panel # 6				
Panel length(ft) = Panel height(ft) =	7.0 8.0	0.00 0.0		0.0	0.0					
Panel height(ft) = Uplift due to lateral load(lb) =	8.0 1763	0.0		0 0	0 0					
Dead load on the panel (lb) =	434	0			0					
Roof tributary(ft		0.0			0.0					
Floor tributary(ft	,	0.0			0.0					
Wall weight(psf)	·	0			0					
Uplift of this floor(lb) =	1329	0	0		0					
Uplift from upper floor(lb) =	0	0	0	0	0	0				
Total hold-down force(lb)=	1329	0	0	0	0	0				
>>> Hold-down Type	STHD14									
			VALL LINE	# 5						
		SHEAR V		<u># 5</u>						
PANEL DESIGN:										
Section a-	Tributary width(ft)	=	46.0		Seismic(plf)	=		Wind(plf)	=	203.4
Section b-	Tributary width(ft)	=	0.0		Seismic(plf)	=		Wind(plf)	=	0
Seismic load ab	()	=	0			Wind load	above this f	loor(lb)	=	0
Total seismic load =	179.5*46/2+0	=	4129 lbs							
Total wind load = Total panel length =	203.4*46/2+0 18.0 ft	=	4678 lbs	•	controls					
Total panel length = Shear =	4678/18.0	=	259.9 lb/ft							
Chical	-1010/10.0	\wedge	200.0 10/10							
>>> Panel type used	3/8" CDX Plywood, Mark-	/10 \	see sheet	SD1 for na	iling shedule					
					Ũ					
					C					
OVERTURNING ANALYSIS:	<u>Panel # 1</u>	 Panel # 2	Panel # 3	Panel # 4	Panel # 5	<u>Panel # 6</u>				
	<u>Panel # 1</u> 4.00	<u>Panel # 2</u> 9.00		<u>Panel # 4</u> 0.0	-	<u>Panel # 6</u> 0.0				
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) =	4.00 8.0	9.00 8.0	5.0 8.0	0.0 0	<u>Panel # 5</u> 0.0 0	0.0 0				
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) =	4.00 8.0 2079	9.00 8.0 2079	5.0 8.0 2079	0.0 0 0	<u>Panel # 5</u> 0.0 0	0.0 0 0				
OVERTURNING ANALYSIS: Panel length(ft) Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) =	4.00 8.0 2079 248	9.00 8.0 2079 730	5.0 8.0 2079 310	0.0 0 0	Panel # 5 0.0 0 0 0	0.0 0 0				
OVERTURNING ANALYSIS: Panel length(ft) Panel height(ft) Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft	4.00 8.0 2079 248) 3.0	9.00 8.0 2079 730 6.0	5.0 8.0 2079 310 3.0	0.0 0 0 0.0	Panel # 5 0.0 0 0 0 0 0.0	0.0 0 0 0 0.0				
OVERTURNING ANALYSIS: Panel length(ft) Panel height(ft) Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft	4.00 8.0 2079 248) 3.0) 0.0	9.00 8.0 2079 730 6.0 0.0	5.0 8.0 2079 310 3.0 0.0	0.0 0 0 0 0.0 0.0	Panel # 5 0.0 0 0 0 0.0 0.0	0.0 0 0 0.0 0.0				
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Vall weight(psf)	4.00 8.0 2079 248) 3.0) 0.0) 16	9.00 8.0 2079 730 6.0 0.0 16	5.0 8.0 2079 310 3.0 0.0 16	0.0 0 0 0.0 0.0 0.0 0.0	Panel # 5 0.0 0 0 0 0.0 0.0 0.0 0.0 0.0	0.0 0 0 0.0 0.0 0.0				
OVERTURNING ANALYSIS: Panel length(ft) Panel height(ft) Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) =	4.00 8.0 2079 248) 3.0) 0.0) 16 1831	9.00 8.0 2079 730 6.0 0.0 16 1350	5.0 8.0 2079 310 3.0 0.0 16 1769	0.0 0 0 0.0 0.0 0.0 0 0 0	Panel # 5 0.0 0 0 0 0.0 0.0 0.0 0.0 0.0 0 0 0 0	0.0 0 0 0.0 0.0 0.0 0 0				
OVERTURNING ANALYSIS: Panel length(ft) Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift for mupper floor(lb) =	4.00 8.0 2079 248 3.0 0) 0.0 0 16 1831 0	9.00 8.0 2079 730 6.0 0.0 16 1350 0	5.0 8.0 2079 310 3.0 0.0 16 1769 0	0.0 0 0 0.0 0.0 0.0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0.0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0.0 0 0 0				
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift from upper floor(lb) = Total hold-down force(lb)=	4.00 8.0 2079 248) 3.0) 0.0 16 1831 0 1831	9.00 8.0 2079 730 6.0 0.0 16 1350 0 1350	5.0 8.0 2079 310 3.0 0.0 16 1769 0 1769	0.0 0 0 0.0 0.0 0.0 0 0 0 0	Panel # 5 0.0 0 0 0 0.0 0.0 0.0 0.0 0.0 0 0 0 0	0.0 0 0 0.0 0.0 0.0 0 0 0				
OVERTURNING ANALYSIS: Panel length(ft) Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift for mupper floor(lb) =	4.00 8.0 2079 248 3.0 0) 0.0 0 16 1831 0	9.00 8.0 2079 730 6.0 0.0 16 1350 0	5.0 8.0 2079 310 3.0 0.0 16 1769 0 1769	0.0 0 0 0.0 0.0 0.0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0.0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0.0 0 0 0				
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift from upper floor(lb) = Total hold-down force(lb)= >>> Hold-down Type	4.00 8.0 2079 248) 3.0) 0.0 16 1831 0 8131 STHD14	9.00 8.0 2079 730 6.0 0.0 1350 1350 STHD14	5.0 8.0 2079 310 3.0 0.0 16 1769 0 1769	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0.0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0.0 0 0 0				
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift from upper floor(lb) = Total hold-down force(lb)= >>> Hold-down Type PANEL DESIGN:	4.00 8.0 2079 248 3.0) 0.0 16 1831 0 1831 STHD14	9.00 8.0 2079 730 6.0 0.0 1350 0 1350 STHD14 SHEAR V	5.0 8.0 2079 310 0.0 16 1769 0 1769 STHD14 VALL LINE	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0 0 0 0 0	275.1	Wind/off)	-	158.2
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift from upper floor(lb) = Total hold-down force(lb)= >>> Hold-down Type PANEL DESIGN: Section a-	4.00 8.0 2079 248) 3.0) 0.0 16 1831 0 1831 STHD14 Tributary width(ft)	9.00 8.0 2079 730 6.0 0.0 16 1350 0 1350 STHD14 SHEAR V =	5.0 8.0 2079 310 3.0 0.0 1769 0 1769 STHD14 VALL LINE 27.0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0 0 0 0 0 0		Wind(plf) Windrolf)	=	158.2 0
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift from upper floor(lb) = Total hold-down force(lb) = >>> Hold-down Type PANEL DESIGN: Section a- Section b-	4.00 8.0 2079 248) 3.0) 0.0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft)	9.00 8.0 2079 730 6.0 0.0 16 1350 0 1350 STHD14 SHEAR V = =	5.0 8.0 2079 310 3.0 0.0 1769 0 1769 STHD14 VALL LINE 27.0 0.0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift from upper floor(lb) = Total hold-down force(lb) = >>> Hold-down Type PANEL DESIGN: Section a- Section b-	4.00 8.0 2079 248) 3.0) 0.0 16 1831 0 1831 STHD14 Tributary width(ft)	9.00 8.0 2079 730 6.0 0.0 16 1350 0 1350 STHD14 SHEAR V =	5.0 8.0 2079 310 3.0 0.0 1769 0 1769 STHD14 VALL LINE 27.0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0		Wind(plf)		
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift from upper floor(lb) = Total hold-down force(lb)= >>> Hold-down Type PANEL DESIGN: Section a- Section b- Seismic load ab	4.00 8.0 2079 248) 3.0) 0.0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 275.1*27/2+0	9.00 8.0 2079 730 6.0 0 1350 0 1350 STHD14 SHEAR V = = =	5.0 8.0 2079 310 3.0 0.0 1769 0 1769 STHD14 VALL LINE 27.0 0.0 0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) Panel height(ft) Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Vall weight(psf) Uplift of this floor(lb) = Uplift form upper floor(lb) = Total hold-down force(lb)= >>> Hold-down Type PANEL DESIGN: Section a- Section b- Seismic load ab Total seismic load =	4.00 8.0 2079 248) 3.0) 0.0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) ove this floor(lb)	9.00 8.0 2079 7300 6.0 0 1350 0 1350 STHD14 SHEAR V = = = =	5.0 8.0 2079 310 3.0 0.0 1769 0 1769 STHD14 VALL LINE 27.0 0 3714 lbs	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift from upper floor(lb) = Total hold-down force(lb)= >>> Hold-down Type PANEL DESIGN: Section a- Section b- Seismic load ab Total seismic load = Total wind load	4.00 8.0 2079 248 3.0 0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 275.1*27/2+0 158.2*27/2+0	9.00 8.0 2079 7300 6.0 0 1350 0 1350 STHD14 SHEAR V = = = =	5.0 8.0 2079 310 3.0 0.0 1769 0 1769 STHD14 VALL LINE 27.0 0 3714 lbs	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift form upper floor(lb) = Total hold-down force(lb)= >>> Hold-down Type PANEL DESIGN: Section a- Section b- Seismic load ab Total seismic load = Total wind load = Total panel length =	4.00 8.0 2079 248) 3.0) 0.0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 275.1*27/2+0 158.2*27/2+0 16.0 ft	9.00 8.0 2079 730 6.0 0 1350 0 1350 STHD14 SHEAR V = = = = =	5.0 8.0 2079 310 3.0 0.0 1769 5THD14 VALL LINE 27.0 0.0 0 3714 lbs 2136 lbs 232.1 lb/ft	0.0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift form upper floor(lb) = Total hold-down force(lb)= >>> Hold-down Type PANEL DESIGN: Section a- Section a- Section b- Seismic load ab Total panel length = Total panel length = Shear = >>> Panel type used	4.00 8.0 2079 248 3.0 0.0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 275.1*27/2+0 158.2*27/2+0 16.0 ft 3714/16.0	9.00 8.0 2079 730 6.0 0.0 1350 0 1350 STHD14 SHEAR V = = = = =	5.0 8.0 2079 310 3.0 0.0 1769 5THD14 VALL LINE 27.0 0.0 0 3714 lbs 2136 lbs 232.1 lb/ft	0.0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) Panel height(ft) Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift from upper floor(lb) = Total hold-down force(lb)= >>> Hold-down Type PANEL DESIGN: Section a- Section b- Setsinic load ab Total seismic load = Total panel length = Shear =	4.00 8.0 2079 248 0.0.0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 275.1*27/2+0 16.0 ft 3714/16.0 3/8" CDX Plywood, Mark-	9.00 8.0 2079 730 6.0 0 0 1350 0 1350 STHD14 SHEAR V = = = = = =	5.0 8.0 2079 310 3.0 0.0 1769 STHD14 VALL LINE 27.0 0.0 0 3714 lbs 2136 lbs 232.1 lb/ft see sheet	0.0 0 0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift for this floor(lb) = Uplift from upper floor(lb) = Total hold-down force(lb)= >>> Hold-down Type PANEL DESIGN: Section a- Section b- Seismic load a= Total seismic load = Total seismic load = Total seismic load = Total panel length = Shear = >>> Panel type used OVERTURNING ANALYSIS:	4.00 8.0 2079 248) 3.0) 0.0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 275.1*27/2+0 158.2*27/2+0 15.0 ft 3714/16.0 3/8" CDX Plywood, Mark- <u>Panel # 1</u>	9.00 8.0 2079 730 6.0 0.0 13500 STHD14 SHEAR V = = = = = = = = = = <u>-</u> 10 <u>Panel # 2</u>	5.0 8.0 2079 310 3.0 0.0 1769 STHD14 VALL LINE 27.0 0.0 0 3714 lbs 2136 lbs 232.1 lb/ft see sheet Panel # 3	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) Panel height(ft) Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Vall weight(psf) Uplift of this floor(lb) = Uplift from upper floor(lb) = Uplift from upper floor(lb) = Total hold-down force(lb) = >>> Hold-down Type PANEL DESIGN: Section a- Section b- Setion b- Total seismic load = Total panel length = Shear = >>> Panel type used OVERTURNING ANALYSIS: Panel length(ft) =	4.00 8.0 2079 248) 0.0) 0.0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 0 275.1*27/2+0 158.2*27/2+0 16.0 ft 3714/16.0 3/8" CDX Plywood, Mark- <u>Panel # 1</u> 4.00	9.00 8.0 2079 7300 6.0 0.0 1350 STHD14 SHEAR V = = = = = = = = = = = = = = = = = = =	5.0 8.0 2079 310 3.0 0.0 1769 0 1769 STHD14 VALL LINE 27.0 0 3714 lbs 2136 lbs 232.1 lb/ft see sheet <u>Panel # 3</u> 4.0	0.0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) Panel height(ft) Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Vall weight(psf) Uplift of this floor(lb) = Uplift from upper floor(lb) = Uplift from upper floor(lb) = Total hold-down force(lb) = >>> Hold-down Type PANEL DESIGN: Section a- Sec	4.00 8.0 2079 248) 3.0) 0.0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 275.1*27/2+0 158.2*27/2+0 15.0 ft 3714/16.0 3/8" CDX Plywood, Mark- <u>Panel # 1</u>	9.00 8.0 2079 730 6.0 0.0 13500 STHD14 SHEAR V = = = = = = = = = = <u>-</u> 10 <u>Panel # 2</u>	5.0 8.0 2079 310 3.0 0.0 1769 STHD14 VALL LINE 27.0 0.0 0 3714 lbs 2136 lbs 232.1 lb/ft see sheet <u>Panel # 3</u> 4.0 8.0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift form upper floor(lb) = Total hold-down force(lb)= >>> Hold-down Type PANEL DESIGN: Section a- Section a- Section b- Section b- Section a- Section b- Section a- Section a- Section a- Section a- Section a- Section b- Setal seismic load = Total panel length = Shear >>> Panel type used OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) =	4.00 8.0 2079 248 3.0 0 0.0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 0 275.1*27/2+0 158.2*27/2+0 16.0 ft 3714/16.0 3/8" CDX Plywood, Mark- <u>Panel # 1</u> 4.00 8.0	9.00 8.0 2079 7300 6.0 0.0 1350 STHD14 SHEAR V = = = = = = = = = = = = 2 8.0 8.0 8.0 8.0 8.0	5.0 8.0 2079 310 3.0 0.0 1769 STHD14 VALL LINE 27.0 0.0 0 3714 lbs 2136 lbs 232.1 lb/ft see sheet <u>Panel # 3</u> 4.0 8.0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Filoor tributary(ft Filoor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Total hold-down force(lb) = Total hold-down force(lb)= >>> Hold-down Type PANEL DESIGN: Section a- Section b- Seismic load ab Total seismic load = Total panel length = Shear = >>> Panel type used OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) =	4.00 8.0 2079 248) 3.0) 0.0 16 1831 STHD14 Tributary width(ft) Tributary width(ft) ove this floor(lb) 275.1*27/2+0 16.0 ft 3714/16.0 3/8" CDX Plywood, Mark- <u>Panel # 1</u> 4.00 8.0 1857 333	9.00 8.0 2079 730 6.0 0.0 1350 STHD14 SHEAR V = = = = = = = = = = = = = = = = = = =	5.0 8.0 2079 310 3.0 0.0 1769 STHD14 VALL LINE 27.0 0.0 0 3714 lbs 2136 lbs 232.1 lb/ft see sheet Panel # 3 4.0 8.0 761	0.0 0 0 0.0 0.0 0 0 0 0 #6 SD1 for na <u>Panel #4</u> 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift form upper floor(lb) = Total hold-down force(lb) = >>> Hold-down Type PANEL DESIGN: Section a- Shear = Total panel length = Shear = >>> Panel type used OVERTURNING ANALYSIS: Panel height(ft) = Panel height(ft) = Duplift due to lateral load(lb) = = Dead load on the panel (lb) = =	4.00 8.0 2079 248 3.0 0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 275.1*27/2+0 168.2*27/2+0 160.0 ft 3714/16.0 3/8" CDX Plywood, Mark- <u>Panel # 1</u> 4.00 8.0 1857 333) 3.0	9.00 8.0 2079 730 6.0 0 0 1350 STHD14 SHEAR V = = = = = = = Panel # 2 8.00 8.0 1857 1521	5.0 8.0 2079 310 3.0 0.0 1769 5THD14 VALL LINE 27.0 0.0 3714 lbs 2136 lbs 232.1 lb/ft see sheet <u>Panel # 3</u> 4.0 8.0 1857 761	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Total hold-down force(lb) = Total hold-down force(lb)= >>> Hold-down Type PANEL DESIGN: Section a- Section a- Section a- Section b- Seismic load ab Total seismic load = Total panel length = Total panel length = Shear = >>> Panel type used OVERTURNING ANALYSIS: Panel length(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Floor tributary(ft Koor tributary(ft Veant weight(psf) Wall weight(psf)	4.00 8.0 2079 248 3.0 0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 275.1*27/2+0 158.2*27/2+0 16.0 ft 3714/16.0 3/8" CDX Plywood, Mark- <u>Panel # 1</u> 4.00 8.0 1857 333 0 0.0 16 16 16 16 16 16 16 16 16 16	9.00 8.0 2079 730 6.0 0.0 1350 STHD14 SHEAR V = = = = = = = = = = <u>10</u> Panel #2 8.00 8.0 1857 1521 15.5 0.0 16	5.0 8.0 2079 310 3.0 0.0 1769 STHD14 VALL LINE 27.0 0.0 0 3714 lbs 2136 lbs 232.1 lb/ft see sheet <u>Panel # 3</u> 4.0 8.0 1857 761 15.5 0.0 0	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift form upper floor(lb) = Uplift form upper floor(lb) = Total hold-down force(lb) = >>> Hold-down Type PANEL DESIGN: Section a- Section b- Section b- Section b- Section b- Section a- Section b- Section a- Section b- Section b- Shear Panel length Shear = >>> Panel type used OVERTURNING ANALYSIS: Panel height(ft) Panel height(ft) = Panel height(ft) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Floor tributary(ft Vall weight(psf) Uplift of this floor(lb) =	4.00 8.0 2079 248 3.0 0.0 16 1831 STHD14 Tributary width(ft) Tributary width(ft) 275.1*27/2+0 16.0 ft 3714/16.0 3/8" CDX Plywood, Mark- <u>Panel # 1</u> 4.00 8.0 1857 333 0.0 0.0 16 1524	9.00 8.0 2079 730 6.0 0 0 1350 STHD14 SHEAR V = = = = - - - - - - - - - - - - -	5.0 8.0 2079 310 3.0 0.0 1769 STHD14 VALL LINE 27.0 0.0 0 3714 lbs 2136 lbs 232.1 lb/ft see sheet <u>Panel # 3</u> 4.0 8.0 1857 761 15.5 0.0 16	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) Panel height(ft) Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Vall weight(psf) Uplift of this floor(lb) = Uplift form upper floor(lb) = Total hold-down force(lb) = >>> Hold-down Type PANEL DESIGN: Section a- Section b- Section b- Section b- Stotal seismic load = Total panel length = Shear = >>> Panel type used OVERTURNING ANALYSIS: Panel ength(ft) = Panel length(ft) = Panel length(ft) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Floor tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift form upper floor(lb) =	4.00 8.0 2079 248 3.0 0.0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 275.1*27/2+0 168.2*27/2+0 16.0 ft 3714/16.0 3/8" CDX Plywood, Mark- <u>Panel # 1</u> 4.00 8.0 1857 333 0.00 1652 4.00 1624 0	9.00 8.0 2079 7300 0.0 1350 STHD14 SHEAR V = = = = = Panel # 2 8.00 8.0 1557 1521 15.5 0.0 16 3360 3360	5.0 8.0 2079 310 3.0 0.0 1769 5THD14 VALL LINE 27.0 0.0 0 3714 lbs 2136 lbs 232.1 lb/ft see sheet <u>Panel # 3</u> 4.0 8.0 1857 761 15.5 0.0 165 761	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0
OVERTURNING ANALYSIS: Panel length(ft) = Panel height(ft) = Uplift due to lateral load(lb) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Wall weight(psf) Uplift of this floor(lb) = Uplift form upper floor(lb) = Uplift form upper floor(lb) = Total hold-down force(lb) = >>> Hold-down Type PANEL DESIGN: Section a- Section b- Section b- Section b- Section b- Section a- Section b- Section a- Section b- Section b- Shear Panel length Shear = >>> Panel type used OVERTURNING ANALYSIS: Panel height(ft) Panel height(ft) = Panel height(ft) = Dead load on the panel (lb) = Roof tributary(ft Floor tributary(ft Floor tributary(ft Vall weight(psf) Uplift of this floor(lb) =	4.00 8.0 2079 248 3.0 16 1831 0 1831 STHD14 Tributary width(ft) Tributary width(ft) 0 1832 STHD14 Tributary width(ft) 275.1*27/2+0 158.2*27/2+0 16.0 ft 3714/16.0 3/8" CDX Plywood, Mark- <u>Panel # 1</u> 4.00 8.0 1857 333 0 0 0 1524	9.00 8.0 2079 730 6.0 0 0 1350 STHD14 SHEAR V = = = = - - - - - - - - - - - - -	5.0 8.0 2079 310 3.0 0.0 1769 5THD14 VALL LINE 27.0 0 3714 lbs 2136 lbs 232.1 lb/ft see sheet <u>Panel # 3</u> 4.0 8.0 1857 761 15.5 0.0 1096	0.0 0 0 0.0 0.0 0 0 0 0 0 0 0 0 0 0 0 0	Panel # 5 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0 0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	Wind(plf)	=	0

SHEAR WALL LINE # 7

PANEL DESIGN:										
Section a-	Tributary width(ft)	=	27.0		Seismic(plf)	=	275.1	Wind(plf)	=	158.2
Section b-	Tributary width(ft)	=	0.0		Seismic(plf)	=	0	Wind(plf)	=	0
Seismic load al	bove this floor(lb)	=	0			Wind loa	ad above th	is floor(lb)	=	0
Total seismic load =	275.1*27/2+0	=	3714 lbs	←	controls					
Total wind load =	158.2*27/2+0	=	2136 lbs							
Total panel length =	16.0 ft									
Shear =	3714/16.0	=	232.1 lb/ft							
		\wedge								
>>> Panel type used	3/8" CDX Plywood, Mark-	/10 \	see sheet	SD1 for na	ailing shedule					
					•					
OVERTURNING ANALYSIS	:									
	Panel # 1	Panel # 2	Panel # 3	Panel # 4	Panel # 5	Panel #	6			
Panel length(ft) =	8.00	8.0	0.0	0.0	0.0	0.	0			
Panel height(ft) =	8.0	8.0	0.0	0	0		0			

Panel length(ft) =	8.00	8.0	0.0	0.0	0.0	0.0
Panel height(ft) =	8.0	8.0	0.0	0	0	0
Uplift due to lateral load(lb) =	1857	1857	0	0	0	0
Dead load on the panel (lb) =	1521	1521	0	0	0	0
Roof tributary(ft)	15.5	15.5	0.0	0.0	0.0	0.0
Floor tributary(ft)	0.0	0.0	0.0	0.0	0.0	0.0
Wall weight(psf)	16	16	0	0	0	0
Uplift of this floor(lb) =	336	336	0	0	0	0
Uplift from upper floor(lb) =	0	0	0	0	0	0
Total hold-down force(lb)=	336	336	0	0	0	0
>>> Hold-down Type	STHD14	STHD14				

CONTINUOUS FOOTING DESIGN

Allowable Soil Bearing pressure = 1000 psf

CONTINUOUS FOOTING at Front of Rear of House

Loading on Continuous Footing:

	Roof load Wall Load Floor Load		35 psf x (27'/2 +2') 16 psf x 8'	= 542.5 plf = 128 plf
	Total Load	=	670.5 plf	
Required Width	n of Footing	=	670.5/1000 0.671'	
	Use: <u>12</u> " wid	e x <u>´</u>	<u>12</u> " deep w/ <u>1-#4</u> reba	rs at top and bottom

FOUNDATION DESIGN

1000 psf

Allowalblw Soil Bearing Pressure =

Allowable Point Load at Continuous Footing:

Pmax = Pa * S * W/144

12" x 12" footing, Pmax = 1000 x 39.5 x 12" / 144 = 3292 LBS

